

## Lesson 08 Outline

* Problem definition and motivations
*Modeling deformable solids with mass-spring model
* Position based dynamics
* Modeling cloths with mass-spring model
* Modeling hair with mass-spring model
* Demos / tools / libs


## Simulation of Deformable Solids

*Lagrangian Mesh Based Methods
$\rightarrow$ Continuum Mechanics Based Methods
$\rightarrow$ Mass-Spring Systems

* Lagrangian Mesh Free Methods
$\rightarrow$ Loosely Coupled Particle Systems
$\rightarrow$ Smoothed Particle Hydrodynamics (SPH)
$\rightarrow$ Mesh Free Methods for the solution of PDEs
* Reduced Deformation Models and Modal Analysis
*Eulerian and Semi-Lagrangian Methods
$\rightarrow$ Fluids and Gases
$\rightarrow$ Melting Objects


## Mass-spring

## Mass-spring Model

*Each deformable solid is modeled as a graph (mesh) of particles (with mass) connected with mass-less springs

* Particle Model
$\rightarrow$ Each particle is defined at least by its Mass (mi), Position (pi), Velocity (vi)
$\Rightarrow$ Additionally there can be force, acceleration, momentum ...
$\rightarrow$ Usually particles can be incident to any number of springs
* Spring Model
$\rightarrow$ Springs usually connects 2 particles and exerts force on them
$\rightarrow$ Usually sprigs have non-zero rest length and some constant material properties


## Hook's Spring Model

*Hook's Law: Strain is directly proportional to stress
*Formally: $f=-k_{s} x$
$\rightarrow x$ is the displacement of the end of the spring from its equilibrium position
$\rightarrow f$ is the restoring force exerted by the material
$\rightarrow k_{s}$ is a material constant called spring stiffness

* Using rest length and velocity damping
* $f=-\left[k_{s}\left(|l|-l_{0}\right)+k_{d}\left(v_{a}-v_{b}\right) /|l|\right](l /|l|)$
$\rightarrow k_{d}$ is damping factor



# Position based <br> <br> Dynamics 

 <br> <br> Dynamics}
$2^{x}$

## Position based Dynamics

* Traditional force based dynamics must solve ODE using some integration scheme. Using simple and fast explicit methods can lead simulation to inaccuracy and instability
* This can be prevented by solving large systems of equations (using implicit methods) or
* Using more geometric approach by directly modify positions into stable and more accurate states.
* Such approach (position based dynamics) gives more control over animation and easily models constraints.


## Position based Dynamics

* Object Representation
$\rightarrow$ We represent dynamic object with a set N vertices
$\rightarrow$ Each vertex has: Mass $\left(m_{i}\right)$, Position ( $p_{i}$ ), velocity ( $v_{i}$ )
* Constraint Representation
$\rightarrow$ Let $\rho=\left(\rho_{1}, \ldots, \rho_{N}\right)$ be the generalized position
$\rightarrow$ The constraint is a functions $C_{j}(\rho)=C_{j}\left(\rho_{1}, \ldots, \rho_{N}\right): R^{3 N} \rightarrow R$
$\rightarrow$ Cardinality $\mathrm{m}_{\mathrm{j}}$ is the number of "used" parameters
$\rightarrow$ Stiffness parameter $k_{j} \in\{0 \ldots 1\}$ is a material property
$\rightarrow$ We define equality (bilateral) constraint as: $C_{j}(\rho)=0$
$\rightarrow$ We define inequality (unilateral) constraint as: $C_{j}(\rho) \geq 0$


## PBD: Algorithm

* 1: forall vertices i: initialize $\rho_{i}=\rho_{i}^{0} ; v_{i}=v_{i}^{0} ; w_{i}=1 / m_{i}$
*2: loop
$\rightarrow$ 3: forall vertices i do $\left\{v_{i} \leftarrow v_{i}+\Delta t w_{i} f_{\text {ext }}\left(x_{i}\right)\right\}$
$\rightarrow 4$ : DampVelocities $\left(\mathrm{v}_{1}, \ldots, \mathrm{v}_{\mathrm{N}}\right)$
$\rightarrow$ 5: forall vertices i do $\left\{q_{i} \leftarrow \rho_{i}+\Delta t v_{i}\right\}$
$\rightarrow$ 6: forall vertices i do \{ CreateCollisionConstraints $\left(x_{i} \rightarrow p_{i}\right)$ \}
$\rightarrow 7$ : loop $n_{S}$ times $\left\{\right.$ ProjectConstraints $\left.\left(C 1, \ldots, C_{M+Q}, q_{1}, \ldots, q_{N}\right)\right\}$
$\rightarrow$ 8: forall vertices I do $\left\{v_{i} \leftarrow\left(q_{i}-p_{i}\right) / \Delta t ; p_{i} \leftarrow q_{i}\right\}$
$\rightarrow$ 9: VelocityUpdate $\left(\mathrm{V}_{1}, \ldots, \mathrm{v}_{\mathrm{N}}\right)$
* 10: endloop


## PBD: Algorithm

* First all masses, positions and velocities are initialized to rest state
* With each simulation frame we do
$\rightarrow$ First we modify velocities due to external forces (3:)
$\rightarrow$ Next we add artificial damping to the system (4:)
$\rightarrow$ Then we predict new positions ( $q_{1}$ ) with simple Euler step (5:)
$\rightarrow$ Next we detect and construct all collision constraints (6:)
$\rightarrow$ We apply "projection" several times on all constraints (7:)
$\rightarrow$ We find correct velocities and set projected positions (8:)
$\rightarrow$ We apply friction and restitution impulses on velocities (9:)


## PBD: Constraint Projection

*Assuming constraint is violated ie. $C(\rho)!=0(<0)$ we must find correction $\Delta \rho$ such that $C(\rho+\Delta \rho)=0(\geq 0)$
*By linearization we get: $C(\rho+\Delta \rho) \approx C(\rho)+\nabla_{\rho} C(\rho) \cdot \Delta \rho$
$\rightarrow$ To conserve both momentums correction must be along direction of constraint function gradient $\nabla_{\rho} C(\rho)$ ie:
$\rightarrow \Delta \rho=\lambda \nabla_{\rho} C(\rho) ; \lambda$ (Lagrange multiplier) is a scalar
$\rightarrow \lambda=-C(\rho) /\left|\nabla_{\rho} C(\rho)\right|^{2 f}$
$\rightarrow$ For i -th particle with mass $\mathrm{m}_{\mathrm{i}}\left(\mathrm{w}_{\mathrm{i}}=1 / \mathrm{m}_{\mathrm{i}}\right)$
$\rightarrow \Delta \rho_{\mathrm{i}}=\lambda \mathrm{w}_{\mathrm{i}} \nabla_{\rho} C\left(\rho_{\mathrm{p}}, \ldots, \rho_{N}\right)$
$\rightarrow \lambda=-w_{i} C\left(\rho_{p}, \ldots, \rho_{N}\right) / \sum_{j} w_{j}\left|\nabla_{\rho j} C\left(\rho_{p}, \ldots, \rho_{N}\right)\right|^{2}$

## PBD: Distance Constraint

$$
\begin{aligned}
& \text { * Let } C(\rho)=C\left(\rho_{1}, \rho_{2}\right)=\left|\rho_{1}-\rho_{2}\right|-d=0 \\
& \quad \rightarrow \nabla_{\rho 1} C\left(\rho_{1}, \rho_{2}\right)=\left(\rho_{1}-\rho_{2}\right) /\left|\rho_{1}-\rho_{2}\right| \\
& \quad \rightarrow \nabla_{\rho 2} C\left(\rho_{1}, \rho_{2}\right)=\left(\rho_{1}-\rho_{2}\right) /\left|\rho_{1}-\rho_{2}\right| \\
& \quad \rightarrow \lambda=\left(\left|\rho_{1}-\rho_{2}\right|-d\right) / w_{1}+w_{2} \quad \text { where } w_{1}=1 / m_{1} \text { and } w_{2}=1 / m_{2} \\
& \rightarrow \Delta \rho_{1}=\left(w_{1} /\left(w_{1}+w_{2}\right)\right)\left(\left|\rho_{1}-\rho_{2}\right|-d\right)\left(\rho_{1}-\rho_{2}\right) /\left|\rho_{1}-\rho_{2}\right| \\
& \quad \rightarrow \Delta \rho_{2}=\left(w_{2} /\left(w_{1}+w_{2}\right)\right)\left(\left|\rho_{1}-\rho_{2}\right|-d\right)\left(\rho_{1}-\rho_{2}\right) /\left|\rho_{1}-\rho_{2}\right|
\end{aligned}
$$

*For equality constraints we always do projection
*For Inequality we project only when $C(\rho)<0$
*Finally we multiply $\Delta \rho$ with stiffness $k$ ( $\Delta \rho k$ )
$\rightarrow$ Due to iterations use $k^{\prime}=1-(1-k)^{\text {vns }}$. Stiffness is applied lineorly after $n_{s}$ iterations

## PBD: Collisions

* Given old position pi and predicted position qi we detect if a ray $\left(\rho_{i}, q_{i}\right)$ enters some object. If yes we compute entry point $\mathrm{a}_{\mathrm{c}}$ and collision normal $\mathrm{n}_{\mathrm{c}}$
*Next add collision constraint with stiffness $k=1$
$C(\rho)=\left(\rho-q_{c}\right) \cdot n_{c} \geq 0$ (ensures non-penetration)
$\rightarrow$ When scene contains more dynamic bodies we must provide constraint from all bodies into one "scene" solver
$\rightarrow$ For triangle meshes with face $\left(\rho_{1}, \rho_{2}, \rho_{3}\right): n_{c}=\left(\rho_{2}-\rho_{1}\right) \times\left(\rho_{3}-\rho_{1}\right)$
$\rightarrow$ Collision constraint generation is done outside the solver loop, to speed up simulation. Artifacts are negligible


## PBD: Damping

*Velocities are damped *Global "body" variables

* forall vertices i
$\rightarrow \Delta \mathrm{v}_{\mathrm{i}}=\mathrm{v}_{\mathrm{cm}}+\omega \times r_{\mathrm{i}}-\mathrm{v}_{\mathrm{i}}$
$\rightarrow \mathrm{v}_{\mathrm{i}} \leftarrow \mathrm{v}_{\mathrm{i}}+\mathrm{k}_{\mathrm{d}} \Delta \mathrm{v}_{\mathrm{i}}$
* endfor
* $\Delta \mathrm{v}_{\mathrm{i}}$ only damps local deviations
$\rightarrow$ Here $v_{c m}+\omega \times r_{i}$ is the velocity due to global body motion
$\rightarrow \rho_{\mathrm{cm}}=\left(\sum_{i} \rho_{i} m\right) /\left(\sum_{i} m\right)$
$\rightarrow v_{\mathrm{cm}}=\left(\sum_{i} v_{i} \mathrm{~m}_{1}\right) /\left(\sum_{i} \mathrm{~m}_{1}\right)$
$\rightarrow L=\sum_{i} r_{i} \times\left(m_{i} v_{i}\right)$
$\rightarrow J=\sum_{i}\left(r^{x}\right)\left(r_{i}^{x}\right)^{\top} m_{i}$
$\rightarrow \omega=J^{-1} \mathrm{~L}$
$\rightarrow r_{i}=\rho_{\mathrm{cm}}-\rho_{\mathrm{i}}$
$\rightarrow r_{i}^{x}$ is cross product matrix


## Position based Dynamics - Summary

* Control over explicit integration with no typical instability problems
* Positions of vertices and objects parts can directly be manipulated during the simulation
*Simple handling of general constraints in the position based setting
*The explicit position based solver is easy to understand and implement.


## Modeling Cloth

## Cloth: Representation

* Cloth is represented with arbitrary manifold triangular mesh (no need for regular lattice)
*Each mesh vertex become a simulation particle
* Given cloth density and thickness we calculate mass of each triangle.
* Mass of each particle is sum of $1 / 3$ of the mass of each adjacent triangle.
* Constraints are defined along edges and faces
* Cloth tearing is performed on vertices with large deformations


## Cloth: Constraints

* Stretching Constraints
$\rightarrow$ Along each mesh edge we define fixed stretching constraint as simple equality distance constraint (spring)
$\rightarrow C_{s}\left(\rho_{1}, \rho_{2}\right)=\left|\rho_{1}-\rho_{2}\right|-l_{0}$ where $I_{0}$ is rest length
$\rightarrow$ Stiffness $\mathrm{K}_{\mathrm{s}}$ is usually higher to overcome springiness
* Bending Constraints
$\rightarrow$ For each pair of adjacent triangles $\left(\rho_{1}, \rho_{3}, \rho_{2}\right)$ and $\left(\rho_{1}, \rho_{2}, \rho_{4}\right)$ we define a bending constraint
$\rightarrow C_{b}\left(\rho_{1}, \rho_{2}, \rho_{3}, \rho_{4}\right)=\operatorname{acos}\left(n_{1}, n_{2}\right)-\varphi_{0}$ where
- $n_{1}=((\rho 2-\rho 1) \times(\rho 3-\rho 1)) /|(\rho 2-\rho 1) \times(\rho 3-\rho 1)|$
- $n_{2}=((\rho 2-\rho 1) \times(\rho 4-\rho 1)) /|(\rho 2-\rho 1) \times(\rho 4-\rho 1)|$



## Cloth: Collisions and Tearing

* Inequality collision constraints is defined as
$* C_{b}\left(q, \rho_{1}, \rho_{2}, \rho_{3}\right)=(q-\rho 1) \cdot n-h$
$\rightarrow q$ is collided point with face $\left(\rho_{1}, \rho_{2}, \rho_{3}\right)$
$\rightarrow n$ is face normal
$\rightarrow h$ - distance to the face.
* Collision with rigid body exerts impulse $m_{i} \rho_{i} / \Delta t$ at $\rho_{i}$
* More involved self-collision detection must be done cloth becomes to be tangled


## Cloth: Overpressure and Tear

* Overpressure inside the closed mesh is modeled as
$\rightarrow C\left(\rho_{1}, \ldots, \rho_{N}\right)=\sum_{j}\left(\rho_{11} \times \rho_{\rho}\right) \cdot \rho_{\beta}-k_{\rho} V_{0}$
$\Rightarrow \nabla_{\rho 1} C=\sum_{j}\left(\rho_{R} \times \rho_{\beta}\right)+\sum_{j}\left(\rho_{\beta 3} \times \rho_{j}\right)+\sum_{j}\left(\rho_{j 1} \times \rho_{\beta}\right)$
* Cloth Tearing Process
$\rightarrow$ Whenever the stretching of an edge exceeds a specified threshold value, we select one of the edge's adjacent vertices
$\rightarrow$ We then put a split plane through that vertex perpendicular to the edge direction and split the vertex into 2 new vertices
$\rightarrow$ All triangles above the split plane are assigned to the original vertex while all triangles below are assigned to the duplicate


## Cloth: Stiffness and Bending


$\left(K_{s} ; k_{b}\right)=(1 ; 0)$
$\left(k_{s} ; k_{b}\right)=(0.5 ; 0)$
$\left(k_{s} ; k_{b}\right)=(0.01 ; 0)$

## Cloth: Self Collisions and Balloons



## Cloth: Examples



## Modeling Hair

## Hair: Representation

* Each hair strand is modeled as a set of vertices connected by edges into series of line segments
*Each vertex is used as simulation particle
* Given material density and strand thickness we can calculate volume/mass of each segment. Particle mass is average of incident edge masses
* Strand constraints are applied along edges, additional (virtual) edges and newly created particles
* Hair tearing is performed on vertices with large deformations


## Hair: Constraints

* We model Curly Hair and Straight Hair
* Stretching Constraints (springs)
$\rightarrow$ Linear springs between every consecutive particle
* Bending Constraints (springs)
$\rightarrow$ Linear springs between every other particle
$\rightarrow$ The edge springs and bending springs together form triangles that implicitly represent the orientation of the hair
* Torsion Constraints (springs)
$\rightarrow$ Twist is modeled by attaching torsion springs that connect each particle to a particle three particles away from it
* Altitude Constraints (springs)
$\rightarrow$ See figure


## Point/Face Altitude Springs


(a) Spring has all non-negative
barycentric weights
(b) Spring has negative barycentric weights
(coplanar)

(c) Degenerate: all point/face springs have negative barycentric weights

## Edge/Edge Altitude Springs


(d) Spring has all non-negative barycentric weights

(e) Spring has negative barycentric weights

(f) Degenerate: all edge/edge springs have negative barycentric weights

## Hair: Altitude Springs

*Point/Face Altitude Springs
$\rightarrow$ Perpendicular to the face starting from the given point
$\rightarrow$ Length is $\mathrm{l}=6 \mathrm{~V} /|\mathrm{u} \times v|$ where $u$ and $v$ are the vectors of the base triangle and V is the signed volume of the tetrahedron
*Edge/Edge Altitude Springs
$\rightarrow$ Perpendicular to common spring and bending spring
$\rightarrow$ Length is $\mathrm{l}=6 \mathrm{~V} /|\mathrm{u} \times \mathrm{v}|$ where u and v are the stretch and bend spring and V is the signed volume of the tetrahedron
$\rightarrow$ For any tetrahedron, the edge/edge or point/face spring with minimal length is guaranteed to have all non-negative barycentric weights, preventing unbounded forces

## (a) Curly Hair Springs



2 Tetrahedra


Edge Springs (desired hair curve)
Extra Edge Springs (form triangles)
Bending Springs (prevent bend)
Torsion Springs (prevent twist)
Tetrahedral Altitude Springs (prevent collapse)
(b) Straight Hair Springs


Figure 7: Straight and curly hair models using edge, bending, torsion, and altitude springs preserving the implied tetrahedra.

## Torsion Spring Path Interrupted



Continuous Torsion Spring Path


Figure 8: Triangles define orientations for penalizing twist, and torsion springs "trace" a continuous path through the nondegenerate triangles - but they are blocked at straight hair segments (left). The subdivision and perturbation of our method removes degeneracies so the path becomes continuous (right).

## Hair: Linear Strands



Figure 9: A simulation of 10,000 long straight hairs with 50 segments each (1,000,000 total particles) on a character shaking his head from side to side.

## Hair: Curly Strands



Figure 14: A simulation of 5,000 long curly hairs with 50 segments each (250,000 total particles) on a character spinning around from back to front.


